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# Experimental and Analytical Study on The Shear Transfer in Composite Post Tensioned Precast Concrete Girders

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## ABSTRACT

This paper proposes a new system for constructing composite post-tensioned precast concrete girders with top slabs where the bottom part is precast, and the top part is cast in place. The experimental study consisted of testing six composite T-girders under two-point loading. The first specimen is post tensioned T-section cast monolithically and acts as a control specimen. In the other five specimens, the web and the girder flange were poured separately and then connected. The investigated variables are the shear connectors' distribution, extended girder stirrups acting as shear connectors, the top slab width, and the concrete strength of the top slabs. Available models from the literature and international code provisions are used for calculating shear transfer failure loads. Based on the obtained results, an analytical study was conducted based on the available model results. This was done to determine the most accurate correlation with the experimental results. The test results showed that using the shear connectors or full stirrups to connect the top slabs to the girders could achieve the total capacity of the monolithic girder. Using shear connectors of 10 mm diameter achieved 100% of the monolithic T-section girder, while using shear connectors of 12 mm diameter achieved 105%. Extending girder stirrups to connect the top slabs to the girders instead of using the shear connectors achieved 100% of the capacity. In addition, increasing the slab width by 50% improved the ductility of the composite T-girders and increased the capacity of the girder by 3%. Moreover, using lower concrete strength for slabs increases slippage between slabs and girders and decreases ultimate girder capacity by 15%. Comparisons between the theoretical results obtained by the available models, codes provisions, and experimental results

were made, and conclusions were drawn. The comparisons showed that the Loov's equation is the least conservative value with the experimental results.

**Keywords:** Post tensioned; Composite concrete girders; Precast concrete; Shear connector; Horizontal shear.

## 1. INTRODUCTION

Composite precast concrete is widely used in bridge construction. It can achieve all structural requirements, including decreasing overall mobilization, increasing construction speed, and maintaining high-quality control [1,2]. The prevailing concept is a deck made almost entirely of prefabricated pieces, such as a full-depth precast bridge deck system [3,4]. Full-depth precast concrete decks are manufactured composite by connecting the deck panels to the supporting beams using different types of shear connections, such as shear studs, bent bars, or threaded rods with nuts [5,6]. These connections are fixed into concrete beams through fabrication or welded to the top flange of the steel beam before or after placing the precast concrete deck slabs [4]. Due to the self-heavy weight and worse tensile strength of normal concrete girders, the full depth precast concrete decks were mainly applied for bridge with steel girder become among the current investigations [7-9]. The disadvantage of this system is that it requires larger quantities of grout material to fill the shear pockets and shear keys [6].

Throughout the years, researchers reported that the behaviour of the interface between the web and the topping slab (flange) of the composite girder affects girder behaviour significantly, as horizontal shear behaviour is crucial for the development of diagonal shear strength, deflection behaviour, and flexural strength to achieve monolithic action [3,10]. The horizontal shear strength of a composite girder mainly depends on the ratio of reinforcement crossing the interface. It also depends on the interface type between the web and flange, and the concrete strength [10-13]. Therefore, shear connectors are required to resist the horizontal shear at the interface surface so that the concrete web and flange act as one unit. Figure 1 illustrates horizontal shearing forces in a composite section [14].

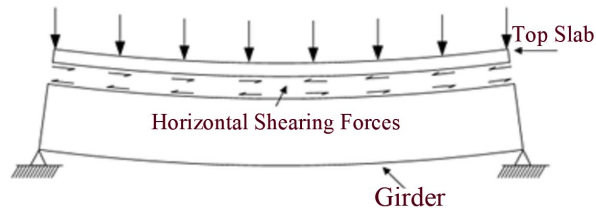


Figure 1: Horizontal shearing forces in a composite section [14]

As resisting horizontal shearing forces develop in the girder and the slab, there is little relative slip between the two surfaces. This may happen due to small cracks along the two interfaces. As the relative slip happens, the shear connectors protruding from the girder into the slab develop tensile forces. They lead to compressive forces through the interface zone and act as horizontal shearing forces. Horizontal shearing forces are transported between the two surfaces by friction due to compressive forces and reinforcement crossing the interface [15]. Figure 2 shows the interface forces developed between the two surfaces due to relative slip [16].

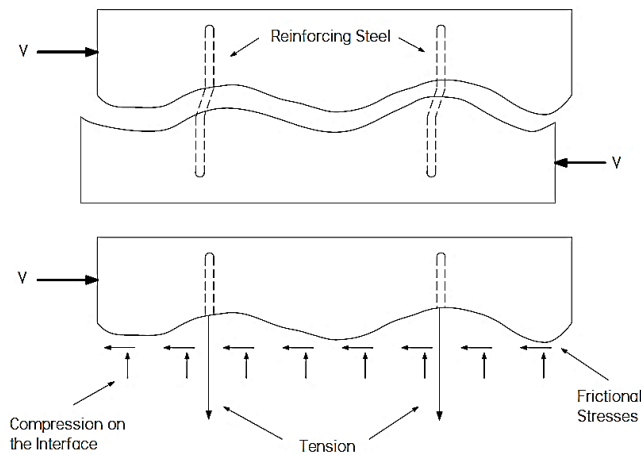


Figure 2: Interface forces between the two surfaces [16]

Several research studies studied the interfacial shear behaviour between ultra-high-performance concrete and normal strength concrete in precast composite members [17-19]. They reported that the shear resistance of the interface was improved by increasing the concrete strength and the degree of surface roughness. They also found that shear reinforcement crossing the interface significantly reduced interface slip before failure. Other researchers studied horizontal shear behaviour between lightweight concrete and normal-weight concrete in concrete composite members [10,20]. They reported that the preparation method of the interface, clamping stress, and the slab's concrete strength substantially affected interface slippage at failure.

They also reported that most composite girders failed in horizontal shear due to horizontal cracks along the interface and separation between the web and the flange.

The distribution of shear connectors is crucial. Throughout the years, there have been many studies and proposed equations to determine the horizontal shear strength of the interface zone in composite sections. Mast was the first to introduce a linear shear friction equation [21]. Birkeland and Birkeland introduced a non-linear function for the ultimate shear capacity of the interface, Birkeland's equation only incorporated a factor times the clamping stress, and nothing accounted for varying surface treatment or concrete strength [22]. Mattock and Hawkins presented a design expression to predict the ultimate longitudinal shear stress and represented the lower bound of the experimental tests. In their previous equation, they reintroduced the concrete strength effect. They also investigated horizontal shear strength for lightweight concrete members [23]. Shaikh proposed a modification to ACI's shear-friction provisions [24], these modifications were incorporated in ACI code 318 [25]. Loov introduced concrete strength influence into the horizontal shear strength equation [26]. Patnaik performed 24 beam tests to study the adequacy of the ACI building code [25] with respect to horizontal shear with a smooth interface. Patnaik stated that it is possible to obtain some nominal shear strength from a smooth interface with no reinforcement, but for design this is not recommended [27].

From the above literature, many researchers studied the behaviour of composite precast concrete members by using several parameters such as the interface surface type, changing the concrete strength by utilizing ultra-high-performance concrete or lightweight concrete, and the ratio of reinforcement crossing the interface. These were carried out for the traditional composite girder systems, which usually consists of a precast beam with a cast-in-place slab [12,13] or a full-depth precast concrete panel system [3-6]. This research proposed a new system for composite precast concrete T-girders. It investigated the behaviour of this system by using several parameters on which no research was cited, such as the combined effects of different shear connector distributions, applying full stirrups to connect the top slab with a supporting beam, changing the top slab width, and changing the compressive concrete strength of top slabs.

## 2. OBJECTIVE AND RESEARCH SIGNIFICANCE

This study proposes a new system for composite post tensioned precast concrete girders with top slabs where the slab's bottom part is precast concrete, and its top part is cast-in-place concrete, as shown in Figure 3. The girders and slabs are cast in the controlled environment of a precast yard prior to construction. They are transferred separately to decrease weight during transport and lifting. Formwork or grout injection will be saved. In addition, there are no large quantities of concrete to be laid and processed on site. This will improve the quality of the concrete and speed up the construction process. All the above factors provide a higher quality product while reducing traffic interruptions. **Figure 4 shows a flowchart for research.**

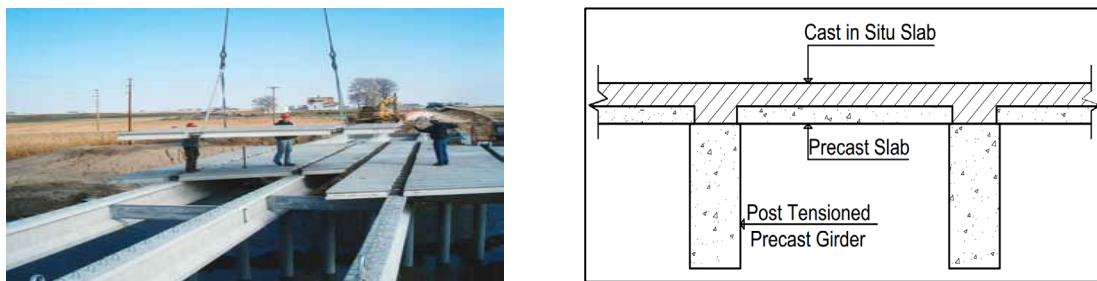
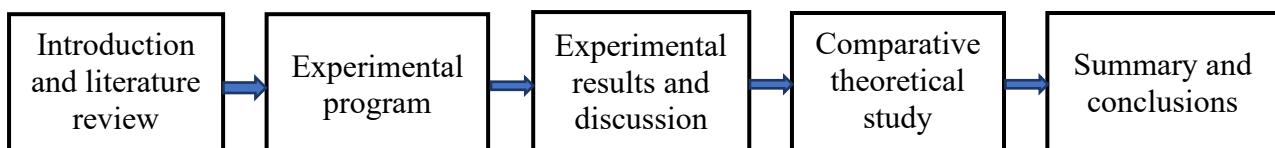


Figure 3: Structural System



**Figure 4: Flowchart for research**

## 3. EXPERIMENTAL PROGRAM

### 3.1 Specimen Details

The experimental program consisted of testing six specimens. The investigated variables are the shear connectors' distribution, extended girder stirrups acting as shear connectors, the top slab width, and the concrete strength of the top slabs. The girder bottom reinforcement was 2D16 mm diameter bars, and the top reinforcement was 2D12 mm diameter bars with a concrete cover of 25 mm. The flange reinforcement was D10 @ 200 mm in both directions. All the specimens were post-tensioned using two prestressing tendons with a 15.24 mm diameter. We reinforced the specimens with closed stirrups of D8 @ 100 mm on the first 500 mm and 125 mm

spacing on the remainder. Special reinforcement at the end zones was provided to prevent splitting and bursts.

Specimen (G1) was cast monolithically and considered a control specimen. Table 1 lists specimen details, and the dimensions are shown in Figure 5. For the rest of the specimens, girder webs and the lower part of topping slabs were cast first separately. Then, the lower part was installed on the girder web, and the rest of topping slab was cast in place. The reinforcement of the bottom and top parts of the slab was D10 @ 200 mm in both directions. Dimensions are shown in Figure 6, and specimens' preparations are shown in Figures 7-15. For all six specimens, post tensioning was applied first.

In Specimen G2, the shear connectors are D10 @ 161 mm, while in Specimen G3, the shear connectors are D12 mm @ 233 mm. In the fourth Specimen (G4), the shear connectors are replaced by full stirrups. The fifth Specimen (G5) is similar to Specimen G2, but the slab width is 750 mm instead of 500 mm. The sixth specimen (G6) is similar to Specimen G2, but the compressive concrete strength for the top slabs is 25MPa instead of 40MPa.

Table 1: Details of test specimens

Girder ID	Description of shear connectors	Shear connectors ratio (%)	Top slab width (mm)	$f_{cu}$ of web girder (MPa)	$f_{cu}$ of slabs (MPa)
G1	Monolithic Construction	-	500	40	40
G2	Ø10@161mm (26 Ø10)	0.405	500	40	40
G3	Ø12@233mm (18 Ø12)	0.405	500	40	40
G4	Full stirrups (Ø8@125mm)	0.698	500	40	40
G5	Ø10@161mm (26 Ø10)	0.405	750	40	40
G6	Ø10@161mm (26 Ø10)	0.405	500	40	25

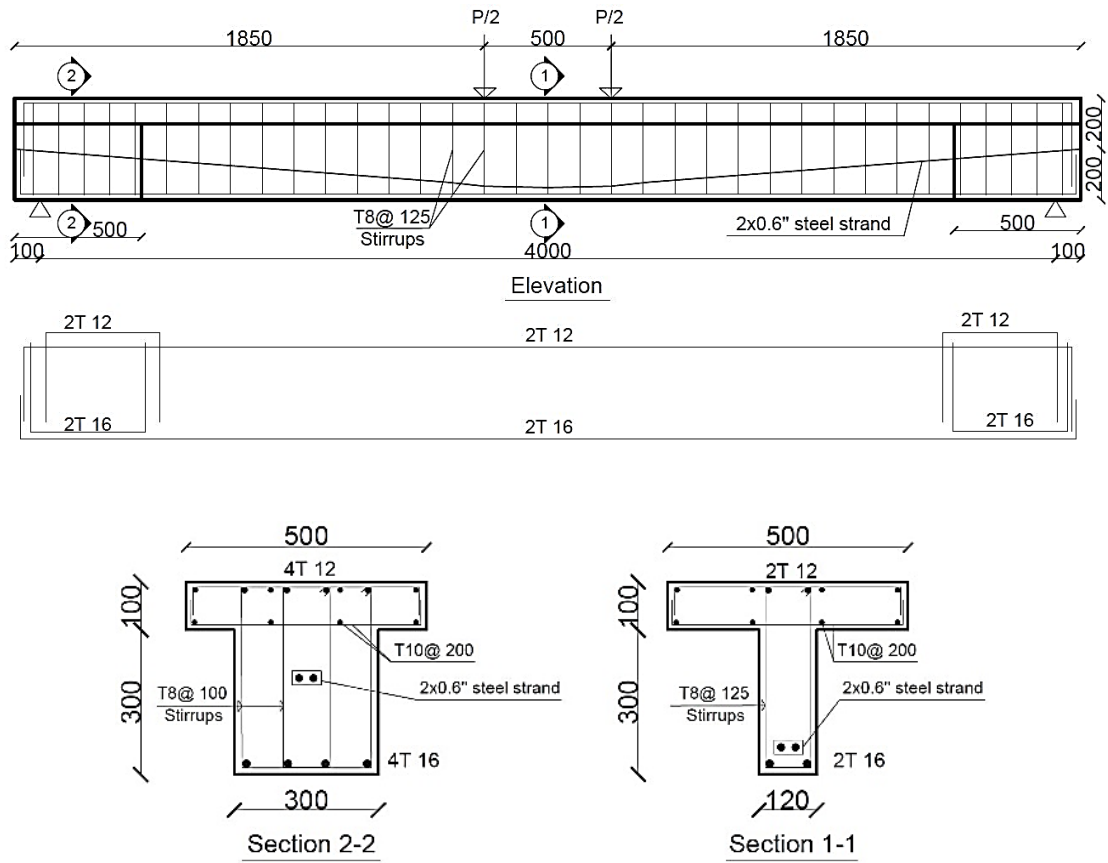


Figure 5: Details of control specimen (G1)

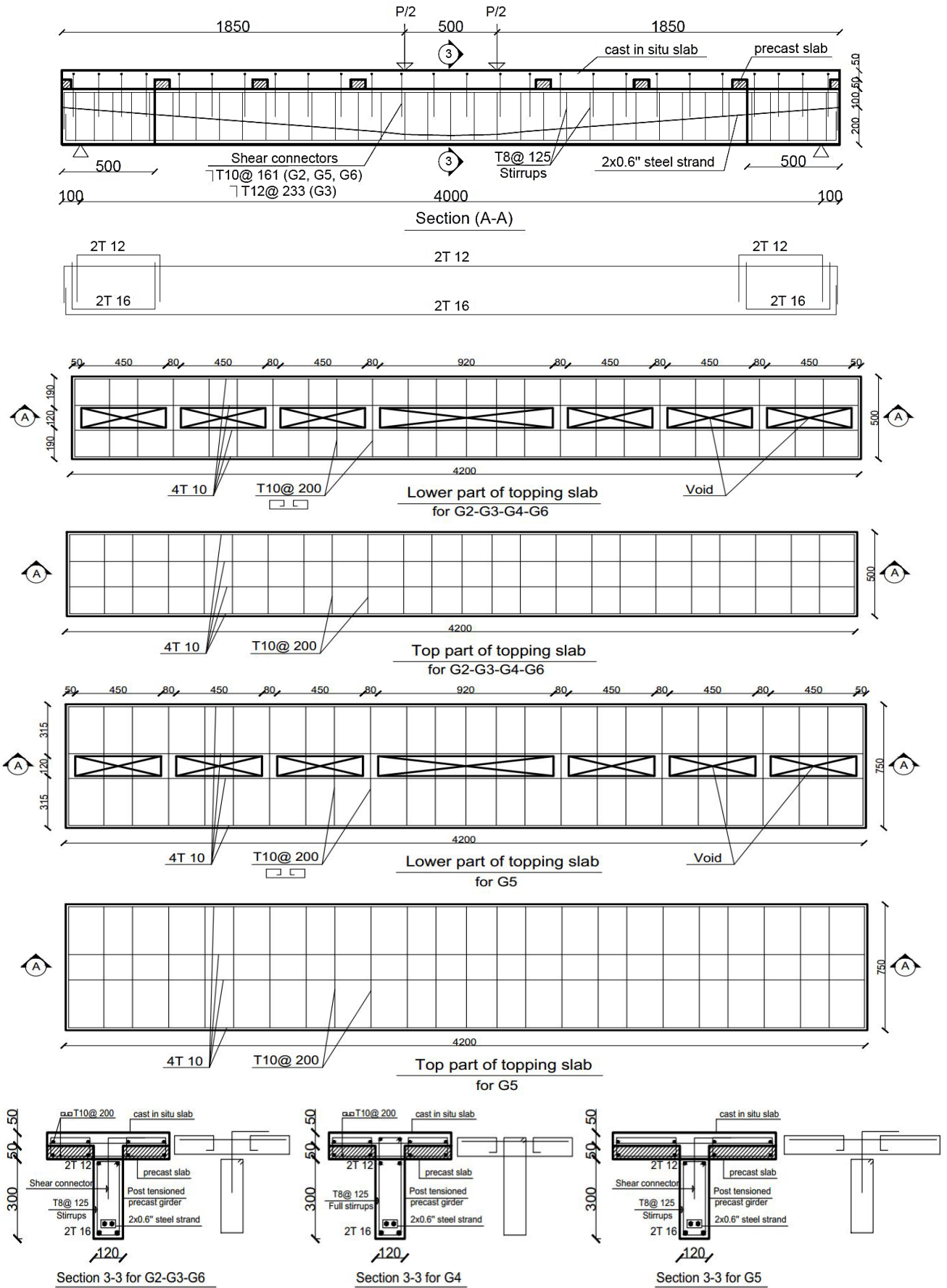


Figure 6: Details of specimens (G2 to G6)



Figure 7: Preparation of formwork for tested specimens



Figure 8: Preparation of reinforcement for tested specimens



Figure 9: Finishing preparation of reinforcement for all specimens



Figure 10: Control specimen G1 and five girder webs



Figure 11: Lower part of topping slab (precast)



Figure 12: Installation of the lower part of topping slab above girder web



Figure 13: Preparation of casting the rest of topping slab



Figure 14: Casting concrete for the rest of topping slab (G2 to G6)



Figure 15: Finishing casting concrete for the rest of topping slab (G2 to G6)

### 3.2 Material Properties

The concrete's designed cube compressive strength was 40 MPa after 28 days. The concrete mix proportion for 40 MPa was 1124 kg/m<sup>3</sup> (coarse aggregates), 630 kg/m<sup>3</sup> (fine aggregates) and 3.5 L/m<sup>3</sup> (Super plasticizer). The water/cement ratio was 0.46, and the cement content was 400 kg/m<sup>3</sup>. The concrete mix proportion for 25 MPa was 1200 kg/m<sup>3</sup> (coarse aggregates) and 800 kg/m<sup>3</sup> (fine aggregates). The water/cement ratio was 0.5, and the cement content was 350 kg/m<sup>3</sup>. Each specimen was cast in one

batch. The reinforcement was high tensile steel with a minimum proof strength of 400 MPa for D10 or more. It was also mild steel with a minimum yield strength of 240 MPa for D8. High-grade steel strands of 15.24 diameter comprising seven individual wires were used. The ultimate tensile strength and the elastic modulus of the steel strands were 1860 MPa and 195000 MPa, respectively. Figure 16 shows the stress-strain diagram of the materials.

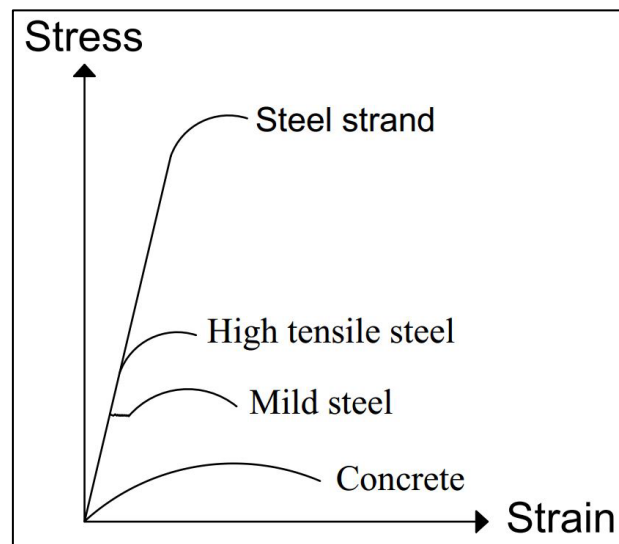


Figure 16: Stress- strain diagram of the materials

### 3.3 Load Setup, Test Procedure, and Instrumentation

The test setup consisted of a structural steel loading frame fixed to a rigid floor. The girders were supported by hinges, and from the other side, by rollers. These supports rested on steel columns anchored to the floor. One load cell of 1000 kN capacity was used during the test. The load was distributed using a rigid steel beam at two concentrated points, as shown in Figure 17. During testing, loading was paused at different load levels to visually inspect the girders for cracks. Cracks were marked on the specimen's surface. Displacements were monitored using linear variable displacement transducers (LVDTs). Figure 18 shows the locations of the LVDTs and strain gauges for a typical girder. The deflection was monitored at three locations, and relative vertical and horizontal movement was monitored at four locations. The steel reinforcement strain was measured by electrical strain gauges. Deflection and strain readings were recorded automatically during the test, using a data acquisition system at each load increment.

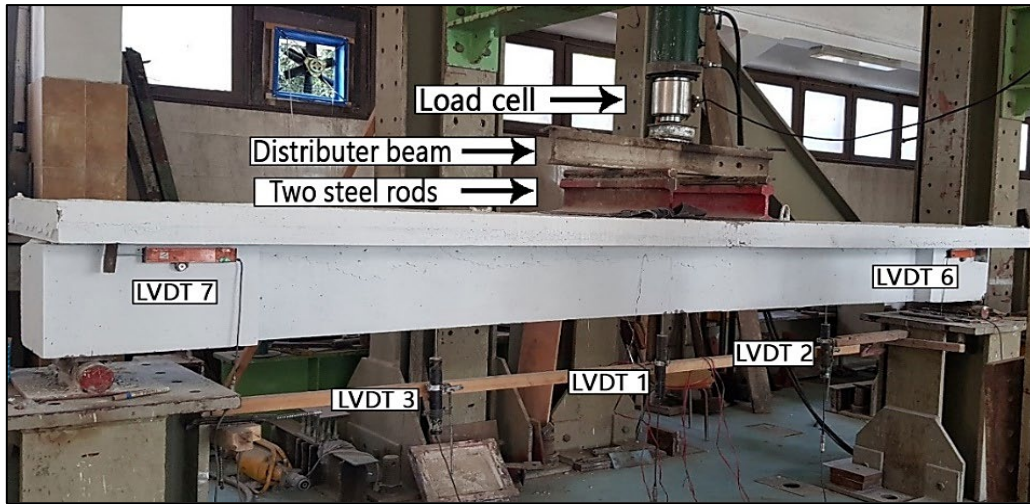


Figure 17: Test set-up for the girders

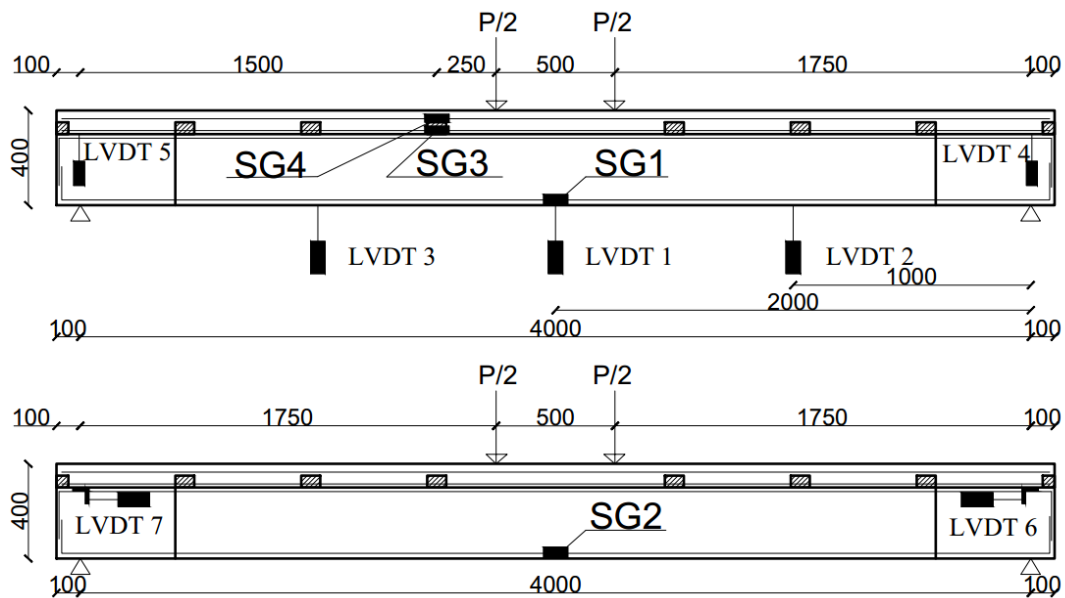


Figure 18: Instrumentation for the girders

#### 4. EXPERIMENTAL RESULTS

The load at first crack and the failure loads were recorded, and the relationship between failure loads and deflection values was drawn. Table 2 summarized the cracking and failure load for all tested specimens.

Table 2: Summary of experimental results for all tested girders

Girder ID	First Crack Load (kN)	Load at First Interfacial Crack (kN)	Failure Load (kN)	Deflection at steel yield (LVDT1) (mm)	Max. Deflection (LVDT1) (mm)	Ductility Index	Max. Strain (SG1)	Failure Mode Shape
G1	70	-	330	25.10	67	2.67	0.019135	flexure followed by crushing at the compression flange
G2	100	210	330	28.88	64.4	2.23	0.019500	The slippage between web and flange at the end girder accompanied by flexure cracks
G3	80	200	348	28.89	62.4	2.16	0.019299	flexure followed by crushing at the compression flange, accompanied by cracks between web and flange at the end girder
G4	70	210	327	27.56	70	2.54	0.019355	flexure followed by crushing at the compression flange, accompanied by cracks between web and flange at the end girder
G5	70	190	340	26.80	67	2.5	0.019055	flexure followed by crushing at the compression flange, accompanied by cracks between web and flange at the end girder
G6	70	190	282	28.63	71	2.48	0.019519	The slippage between web and flange at the end girder accompanied with flexure cracks

#### 4.1 Crack Pattern and Failure Mode

Figures 19 and 20 show the tested girders' cracking patterns and failure modes. In control Specimen G1, the cracks initiated at the mid-span of the girder web increased in number and width by increasing the load up to failure. Horizontal cracks appeared at the web and flange interfaces for all composite girders. The failure in specimens G3 and G4 was due to tensile flexure. Many horizontal cracks with smaller widths appeared at the interface between the web and the flange. However, the vertical cracks widened at the mid-span of the girder web, and the top flange was crushed, as shown in the figures. In specimens G2 and G6, the horizontal cracks increased in

number and width, leading to failure due to slippage between the web and flange at the end girder. In addition, many vertical cracks with smaller widths were present at the girder web mid-span. In Specimen G5, which had a wider slab, many horizontal cracks with smaller widths appeared at the interface between the web and the flange. However, the failure occurred flexibly followed by crushing at the compression flange. This seems to agree with researchers in the literature who observed similar crack propagation in their experimentally studied composite prestressed concrete girders [10,11,27].



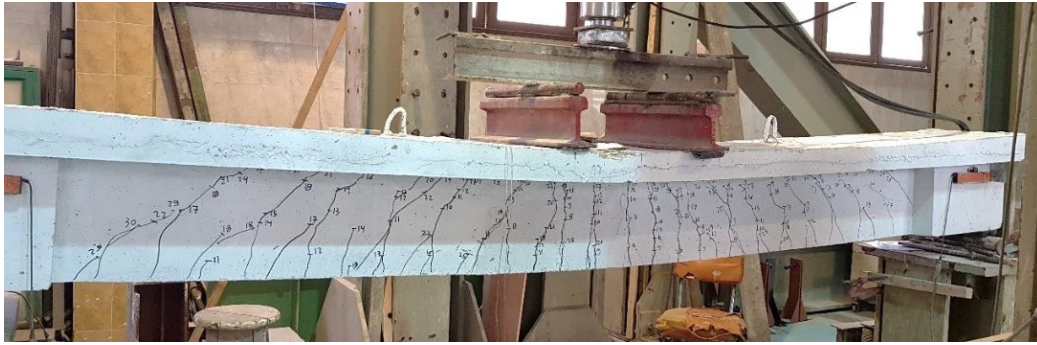
a) Specimen G1



b) Specimen G2



c) Specimen G3



d) Specimen G4



e) Specimen G5

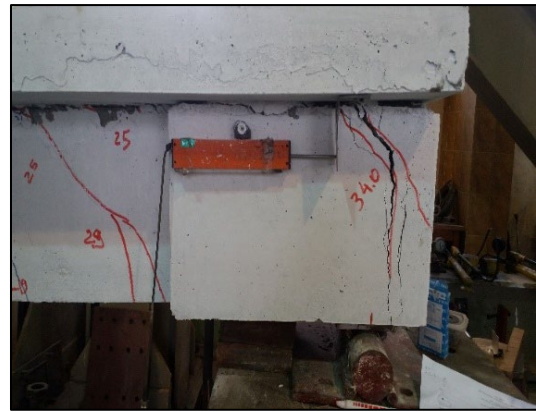


f) Specimen G6

Figure 19: Cracking patterns of tested specimens



a) Specimen G1



b) Specimen G2



c) Specimen G3



d) Specimen G4



e) Specimen G5



f) Specimen G6

Figure 20: Failure modes of tested specimens

#### 4.2 Failure Load and Deformations

Figures 21 and 22 show the relationship between loads and vertical deflections. All girders pass through three stages. At each of the three stages, the load-deflection relation slope changes. The first stage is pre-cracking, where the relation between the load and vertical deflection varies linearly. At Stage Two, where the relation varies linearly and the slope changes due to the loss of sectional stiffness by cracking, the loss of stiffness is constant until the yielding point of strands is reached. Finally, at

Stage Three or the plastic phase, the slope of the relationship is reduced due to yielding and the wide cracks until the failure point. The ductility index is the ratio between the deflection at the ultimate load and the deflection measured when the steel reaches yield strain.

The ultimate load of specimen G2 is the same as that of control specimen G1. At the same time, the ductility index and maximum deflection of specimen G2 are lower than those of control specimen G1 by 16.48% and 3.88%, respectively. It can be noted that using shear connectors 10mm in diameter almost achieved the same results as the control specimen.

The ultimate load of specimen G3 is greater than specimens G1 and G2 by 5.45%. The ductility index and maximum deflection of specimen G3 are lower than specimen G1 by 19.1% and 6.86%. They are also lower than specimen G2 by 3.13% and 3.1%, respectively. This can be attributed to using shear connectors 12mm in diameter, increasing the stiffness of specimen G3 compared to the control specimen.

The ultimate load and ductility index of specimen G4 is lower than those of control specimen G1 by 1% and 4.87%, respectively. The maximum deflection of G4 is higher than that of the control specimen by 4.48%. In addition, the ultimate load of Specimen G4 is lower than Specimens G2 and G3 by 1% and 6.03%, respectively. The ductility index and maximum deflection of Specimen G4 are higher than those of G2 by 13.9% and 8.7%, and higher than those of G3 by 17.6% and 12.18%, respectively. It can be noted that extending girder stirrups to connect the top slabs to the girder instead of using shear connectors almost achieved similar results to the control specimen.

In specimen G5, which had a wider slab of 750 mm instead of 500 mm, the ultimate load is higher than that of G2 by 3.03%. In addition, the ductility index and maximum deflection of G5 are higher than G2 by 12.11% and 4.03%, respectively. This can be attributed to the increasing stiffness of specimen G5 due to the increasing slab width compared to the control specimen.

Specimen G6, which had a lower concrete strength for the top slabs of 25 MPa instead of 40 MPa, the ultimate load is lower than that of G2 by 14.54%. However, it achieved a higher ductility index and maximum deflection than G2 by 11.21% and 10.25%, respectively. This can be attributed to the composite girder's horizontal shear

strength. This mainly depends on the concrete strength at the interface compared to the control specimen.

Again, the ultimate loads, deflections, and ductility were similar to those observed by other researchers in the literature who studied composite girders [10,11,27].

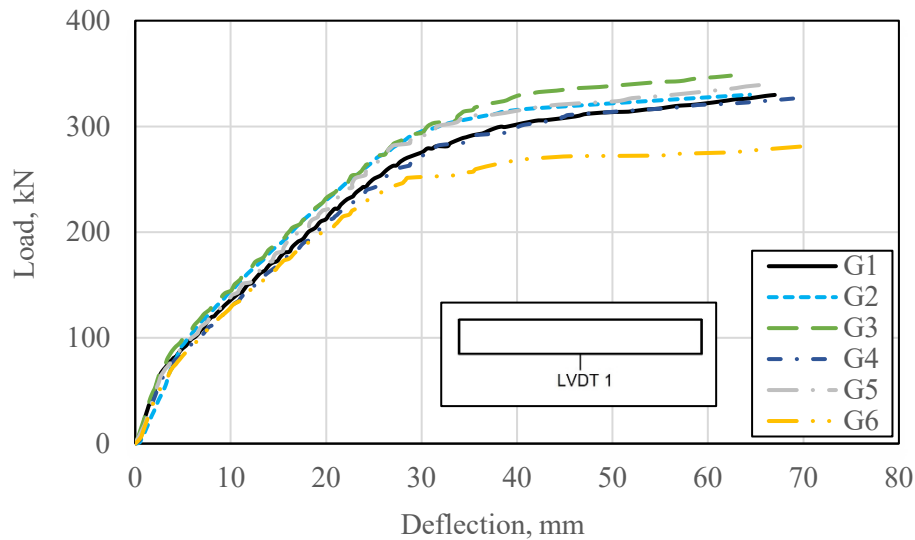


Figure 21: Load – Vertical Deflection Relationship at LVDT 1

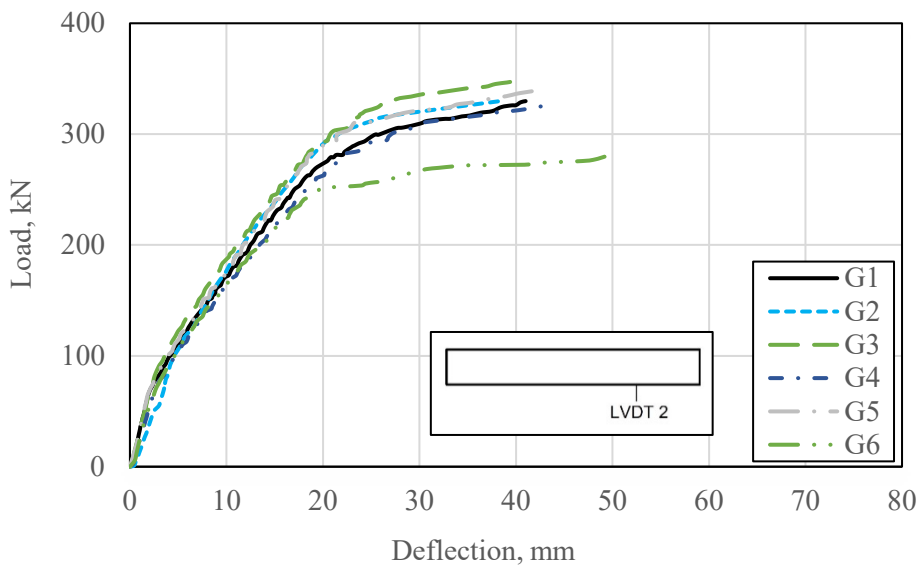


Figure 22: Load – Vertical Deflection Relationship at LVDT 2

Figure 23 shows the relative horizontal displacement between the web and the slab. The girder with lower concrete strength for the top slabs (G6) experienced more relative horizontal displacement than the other girders due to the shear resistance of the interface in the composite girders depending on concrete strength. The reinforcing bars across the interface were ineffective in this case for providing the maximum shear resistance and rigidity prior to the slip. This seems to agree with the researchers

who studied the effect of changing concrete strength in their study. They found that the mechanical bonding strength and shear resistance of the interface increased by increasing the concrete strength of slab [10,17-20].

For girders with the same area of shear connectors (G2 and G3), G2 experienced more relative horizontal displacements than G3. This may be attributed to the higher stiffness of the 12 mm bars, which governs girder behaviour. Specimen G5, which had a wider slab, experienced less relative horizontal displacement at the interface than specimen G2. This may be attributed to the high stiffness of the wide flange. This decreases slab deflection and relative horizontal displacement.

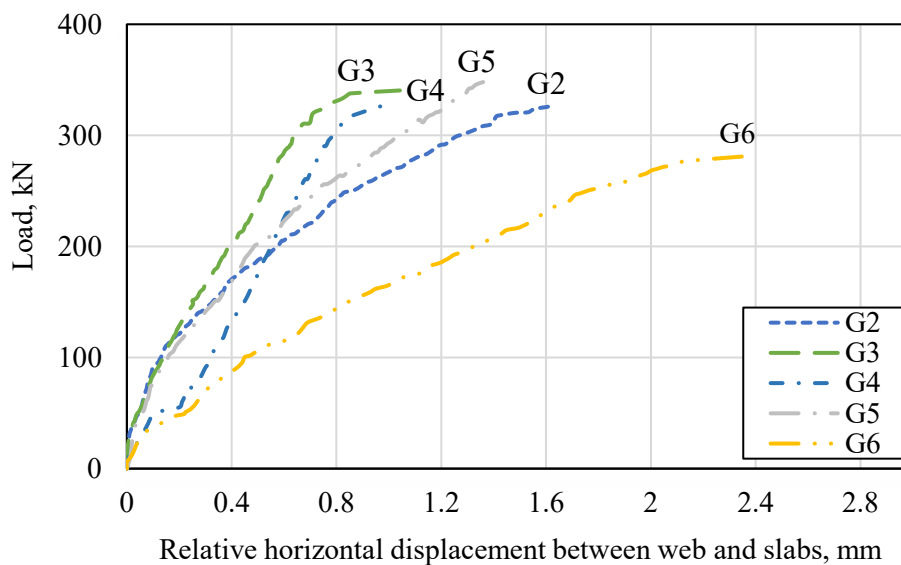


Figure 23: Load –Relative Horizontal Displacement Relationship

### 4.3 Failure load and strain

Figure 24 shows the relationship between the load and the longitudinal steel strains measured at the mid-span. It can be noticed that the maximum steel strain is almost the same for all girder specimens due to the same reinforcement ratio, the strain prior to interface cracking was close to the yield strain.

Figures 25a-f show the strain distribution through the cross-section depth at different loading levels for each specimen. The strain distribution was drawn by connecting SG1, SG3, and SG4 readings in specimen G1. For the rest of the specimens, the neutral axis was determined at different loading levels by measuring the crack length from the experimental work. The neutral axis was assumed above the end of crack.

Then a line was plotted from SG1 to the neutral axis and extended to the end of the web girder. A line was plotted from SG3 to SG4.

It can be seen from Figure 18 that, for all composite girders except G6, the strain distribution was almost continuous at the interface of the web and the slab, especially at the early stages of loading, which indicating full shear interaction between the web and slab. However, as the load increased, the small cracks at the interface were due to the relative slip between the web and slab. The discontinuity of the strain at the interface became more pronounced, indicating a partial shear interaction. It can be concluded that all composite girders except Specimen G6, almost have full composite action. This is in agreement with Wang, who observed that the strain distribution through the depth of cross-section is linear at the stage before the cracks load, and it subsequently became nonlinear because of the cracks emerging by increasing the load [20].

For Specimen G6, the strain distribution at the early stages of loading is almost continuous, indicating full shear interaction between the web and slab. However, as the load increased, the relative slippage between the web and the flange occurred, then the two members acted as a non-composite section and resisted the load as two separate members.

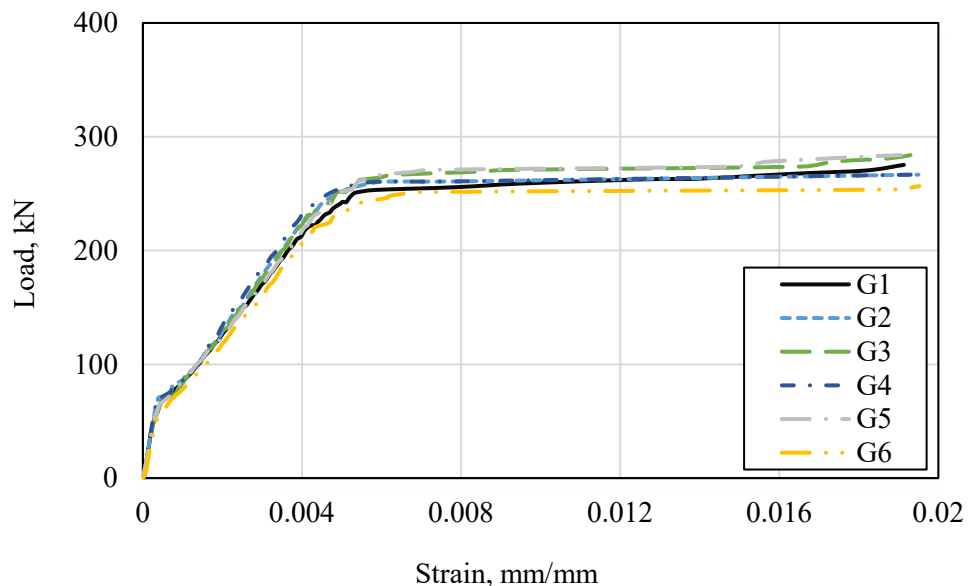
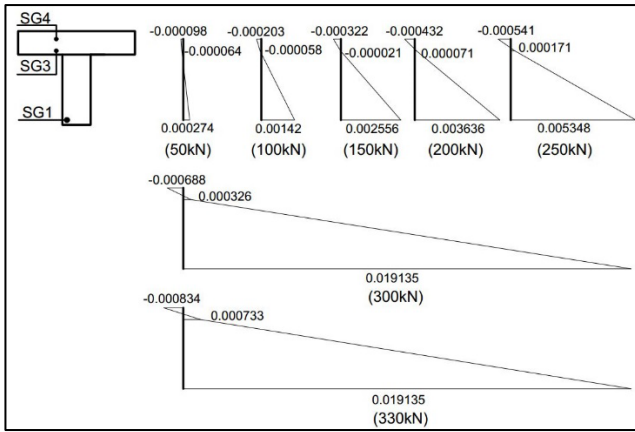
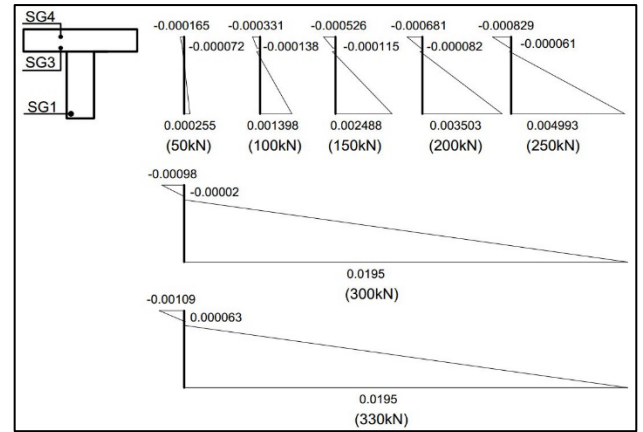


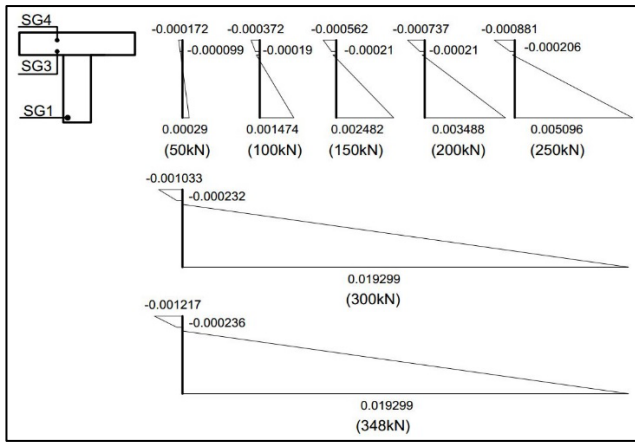
Figure 24: Load – Longitudinal Strain Relationship at the Mid-Span



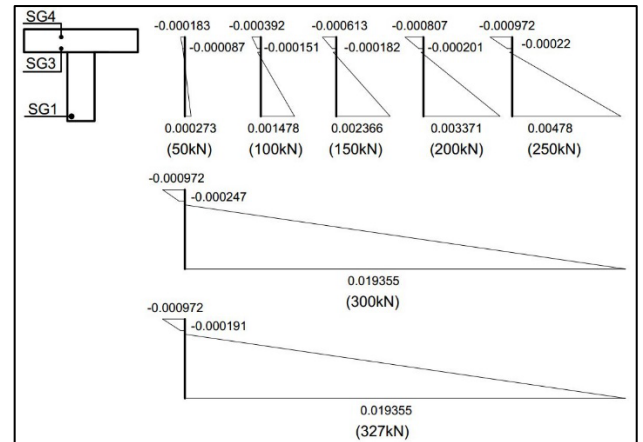
a) Strain Distribution for Specimen G1



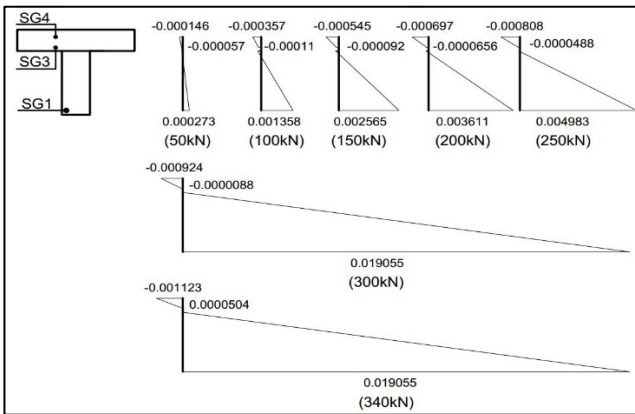
b) Strain Distribution for Specimen G2



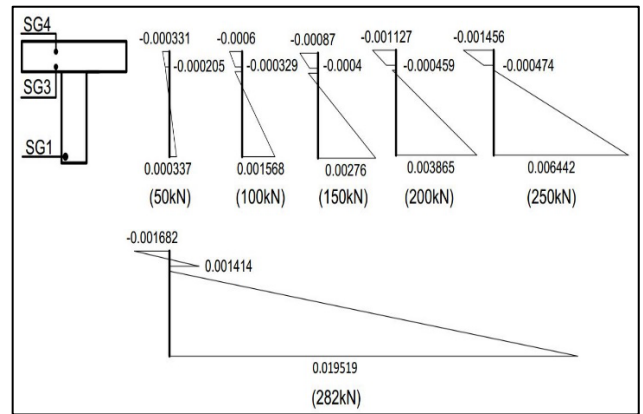
c) Strain Distribution for Specimen G3



d) Strain Distribution for Specimen G4



e) Strain Distribution for Specimen G5



f) Strain Distribution for Specimen G6

Figure 25: Strain Distributions

## 5. Comparative theoretical study

Horizontal shear strength values were calculated using available models from the literature and codes provisions. Many proposed equations have been developed to determine the horizontal shear strength of the interface zone in composite sections. A summary of the variables considered in the equations of codes provisions and models is presented in Table 3. It can be noticed that all codes provisions and model equations consider clamping stress. It can also be noticed that AASHTO LRFD2010 [28], Eurocode-2 [29], ECP 203-2020 [30], Mattock [23] and Patnaik [27] take into account cohesion. In addition, Loov's model [26] is the only equation based on reinforcement strength and concrete.

Table 3: Considered Variables in the Different Analytical Models

Variable	Mast [21]	Birkland [22]	Mattock [23]	Shaikh [24]	Loov [26]	Patnaik [27]	AASHTO [28]	Eurocode-2 [29]	ECP [30]	BS [31]
$f_c$	N	N	N	N	Y	N	N	N	N	N
$f_y$	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y
$\rho_v$	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y
$\mu$	Y	N	Y	Y	N	Y	Y	Y	Y	N
C	N	N	Y	N	N	Y	Y	Y	Y	N

\*Y: Yes

\*N: No

where

$f_c$  is the cylindrical concrete strength.

$f_y$  is the reinforcement yield strength.

$\rho_v$  is the ratio of the steel crossing interface (shear connectors ratio) =  $(A_{vf} / A_c)$ , where  $A_{vf}$  is the area of reinforcement crossing interface (shear connectors area) and  $A_c$  is the area of the cracked interfacial surface.

$\rho_v = 0.405\%$  for specimens G2, G3, G5, G6, and  $\rho_v = 0.698\%$  for specimens G4.

$\mu$  is the coefficient of friction at the interface, which depend on the interface's roughness.

C is the cohesion factor which depends on the roughness of the interface.

Table 4 compares the experimental results and the interfacial shear failure loads calculated from previous research in the literature and design codes. Figure 26 summarises the experimental results and the interfacial shear failure loads calculated from the analytical study. It was found that the equations of Mast [21], BS 8110 [31],

Eurocode-2 [29], ECP 203-2020 [30], and Patnaik [27] are conservative for determining the horizontal shear stress due to the conservative values for cohesion and interfacial friction. Mattock [23] and Shaikh [24]'s equations are less conservative for determining the horizontal shear stress due to the high contribution of cohesion and friction in those equations. In this case, Loov [26], Birkeland [22], and AASHTO LRFD [28] represent the least conservative equation.

The proposed equations are as follows:

- Mast equation [21]  $V_n = \rho_v \cdot f_y \cdot \mu$  (1)

where  $\mu = 1$

- Birkeland equation [22]  $V_n = 2.78 \sqrt{\rho_v \cdot f_y}$  (MPa) (2)

- Mattock equation [23]  $V_n = C + 0.8(\rho_v \cdot f_y + \sigma_n)$  (MPa) (3)

where  $C = 1.38$ ,  $\sigma_n = 0$

- Shaikh equation [24]  $V_n = \lambda \sqrt{6.9 \phi \cdot \rho_v \cdot f_y} \leq 0.25 f_c' \lambda^2$  and  $6.9 \lambda^2$  (MPa) (4)

where  $\lambda$  is the constant used to account for the effect of concrete density ( $\lambda = 1$ ) for normal weight concrete, and  $\phi$  is the strength reduction factor for shear ( $\phi = 0.85$ ).

- Loov equation [26]  $V_n = k \sqrt{\rho_v \cdot f_y \cdot f_c'}$  (MPa) (5)

where  $k$  is constant ( $k = 0.5$  was suggested for an initially un-cracked interface).

- Patnaik equation [27]  $V_n = C + \rho_v \cdot f_y \leq 0.2 f_c'$  and 5.5 MPa (6)

where  $C = 0.60$

- AASHTO LRFD 2010 [28]  $V_n = C + \mu \cdot \rho_v \cdot f_y$  (MPa) (7)

where  $C = 1.90$ ,  $\mu = 1$

- Eurocode-2 [29]  $V_n = C f_{ct} + \mu \cdot \rho_v \cdot f_y$  (MPa) (8)

where  $C = 0.77$ ,  $\mu = 0.60$

- ECP203-2020 [30]  $V_n = 1.35 + 0.5 \cdot \rho_v \cdot f_y$  (MPa) (9)

- BS 8110-1997 [31]  $V_n = \rho_v \cdot f_y$  (10)

Table 4: Comparison of experimental results versus using equations of previous researchers and design codes

Equation	Girder ID	$f_c$ (MPa)	$f_y$ (MPa)	$\rho_v$ %	$\mu$	C	$V_n$ (MPa)	$P_{ver.}$ (kN)	$P_{exp.}$ (kN)	$P_{exp.}/P_{ver.}$	%Con.
Mast equation [21]	G2	-	400	0.405	1	-	1.62	140.02	330	2.36	135.68
	G3	-	400	0.405	1	-	1.62	139.59	348	2.49	149.29
	G4	-	240	0.698	1	-	1.68	144.76	327	2.26	125.88
	G5	-	400	0.405	1	-	1.62	140.02	340	2.43	142.82
	G6	-	400	0.405	1	-	1.62	140.02	282	2.01	101.40
Birkeland equation [22]	G2	-	400	0.405	-	-	3.54	305.77	330	1.08	7.92
	G3	-	400	0.405	-	-	3.53	305.31	348	1.14	13.98
	G4	-	240	0.698	-	-	3.60	310.91	327	1.05	5.18
	G5	-	400	0.405	-	-	3.54	305.77	340	1.11	11.19
	G6	-	400	0.405	-	-	3.54	305.77	282	0.92	-7.78
Mattock equation [23]	G2	-	400	0.405	0.8	1.38	2.68	231.25	330	1.43	42.70
	G3	-	400	0.405	0.8	1.38	2.67	230.91	348	1.51	50.71
	G4	-	240	0.698	0.8	1.38	2.72	235.04	327	1.39	39.12
	G5	-	400	0.405	0.8	1.38	2.68	231.25	340	1.47	47.03
	G6	-	400	0.405	0.8	1.38	2.68	231.25	282	1.22	21.95
Shaikh equation [24]	G2	-	400	0.405	-	-	3.08	266.37	330	1.24	23.89
	G3	-	400	0.405	-	-	3.08	265.97	348	1.31	30.84
	G4	-	240	0.698	-	-	3.13	270.85	327	1.21	20.73
	G5	-	400	0.405	-	-	3.08	266.37	340	1.28	27.64
	G6	-	400	0.405	-	-	3.08	266.37	282	1.06	5.87
Loov equation [26]	G2	34	400	0.405	-	-	3.71	320.68	330	1.03	2.91
	G3	34	400	0.405	-	-	3.71	320.18	348	1.09	8.69
	G4	34	240	0.698	-	-	3.77	326.06	327	1.00	0.29
	G5	34	400	0.405	-	-	3.71	320.68	340	1.06	6.03
	G6	21.25	400	0.405	-	-	2.93	253.52	282	1.11	11.24
Patnaik equation [27]	G2	-	400	0.405	1	0.6	2.22	191.86	330	1.72	72.00
	G3	-	400	0.405	1	0.6	2.22	191.43	348	1.82	81.79
	G4	-	240	0.698	1	0.6	2.28	196.60	327	1.66	66.32
	G5	-	400	0.405	1	0.6	2.22	191.86	340	1.77	77.21
	G6	-	400	0.405	1	0.6	2.22	191.86	282	1.47	46.98
AASHTO LRFD 2010 [28]	G2	-	400	0.405	1	1.9	3.52	304.18	330	1.08	8.49
	G3	-	400	0.405	1	1.9	3.52	303.75	348	1.15	14.57
	G4	-	240	0.698	1	1.9	3.58	308.92	327	1.06	5.85
	G5	-	400	0.405	1	1.9	3.52	304.18	340	1.12	11.77
	G6	-	400	0.405	1	1.9	3.52	304.18	282	0.93	-7.29
Eurocode-2 [29]	G2	-	400	0.405	0.6	0.77	1.74	150.54	330	2.19	119.21
	G3	-	400	0.405	0.6	0.77	1.74	150.28	348	2.32	131.56
	G4	-	240	0.698	0.6	0.77	1.78	153.39	327	2.13	113.19
	G5	-	400	0.405	0.6	0.77	1.74	150.54	340	2.26	125.85
	G6	-	400	0.405	0.6	0.77	1.74	150.54	282	1.87	87.32
ECP203-2020 [30]	G2	-	400	0.405	0.5	1.35	2.16	186.65	330	1.77	76.80
	G3	-	400	0.405	0.5	1.35	2.16	186.44	348	1.87	86.66
	G4	-	240	0.698	0.5	1.35	2.19	189.02	327	1.73	73.00
	G5	-	400	0.405	0.5	1.35	2.16	186.65	340	1.82	82.16
	G6	-	400	0.405	0.5	1.35	2.16	186.65	282	1.51	51.08
BS 8110-1997 [31]	G2	-	400	0.405	-	-	1.62	140.02	330	2.36	135.68
	G3	-	400	0.405	-	-	1.62	139.59	348	2.49	149.29
	G4	-	240	0.698	-	-	1.68	144.76	327	2.26	125.88
	G5	-	400	0.405	-	-	1.62	140.02	340	2.43	142.82
	G6	-	400	0.405	-	-	1.62	140.02	282	2.01	101.40

where  $V_n$  is the ultimate horizontal shear stress,  $P_{ver.}$  is the vertical ultimate load (theoretical), and  $P_{exp.}$  is the experimental failure load.

$$\% \text{ Con.} = (\% \text{ Conservatism}) = \frac{(\text{Experimental result} - \text{Analysis result})}{\text{Analysis result}} \times 100$$

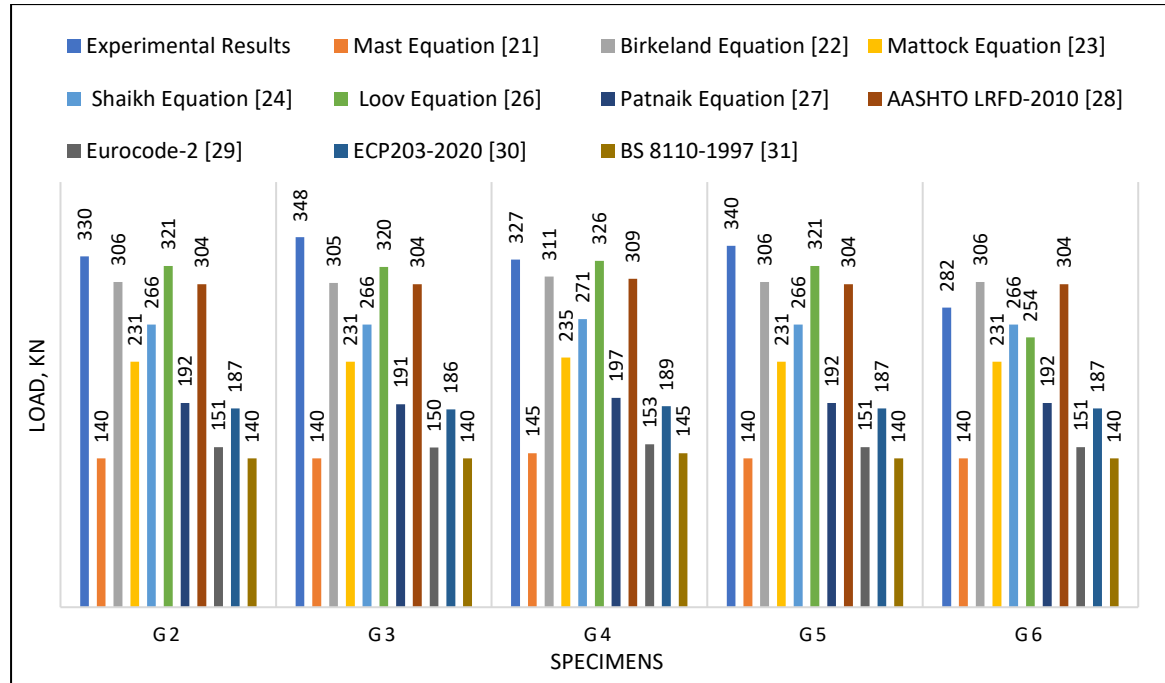


Figure 26: Comparison between experimental results and previous research and codes

## 6. Summary and Conclusions

The current study tested six composite T-girders to evaluate the composite behaviour of post tensioned precast concrete girders with top slabs. The bottom slab is precast, and the top part is cast in place. Among the variables studied were the distribution of shear connectors, the extension of girder stirrups to act as shear connectors, the top slab's width, and the compressive concrete strength of the top slabs. The following conclusions are summarized in the following paragraphs.

Shear connectors are used to connect the top slabs to the girders. This achieves almost the full composite action as the monolithic T-section girder since the shear connectors can provide the ultimate horizontal shear strength at the interface of the top slabs and the girders. For the same shear connector reinforcement ratio, the larger diameter of shear connectors shows higher capacity than the smaller diameter due to the higher stiffness of the larger bars.

Shear connectors of 10 mm diameter achieved 100% of the monolithic T-section girder. However, failure occurred due to slippage between the girder and topping slab

while using shear connectors of 12 mm diameter achieved 105% of the monolithic T-section girder and failure occurred as the monolithic T-section girder.

Extending girder stirrups to connect the top slabs to the girders instead of using shear connectors, achieved almost the full composite action as the monolithic T-section girder, and shows better ductility compared with using the shear connectors. Increasing the top slab width by 50% leads to increasing the capacity of the girder with ratio 3% and improved the ductility of the composite T-girder.

Reducing the concrete strength of topping slabs from 40 MPa to 25 MPa leads to decreasing the ultimate capacity of the girder by 15% and increasing slippage between top slabs and girders.

It was found that predicting equations of Mast [21], BS 8110 [31], Eurocode-2 [29], ECP 203-2020 [30], and Patnaik [27] represent the most conservative equations for determining horizontal shear stress due to the conservative values for cohesion and interfacial friction. Equations of Mattock [23] and Shaikh [24] provide moderate conservative equations for determining the horizontal shear stress due to the high contribution of cohesion and friction in those equations. Equations of Loov [26], Birkeland [22], and AASHTO LRFD [28] represent the least conservative equation.

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### **Compliance with Ethical Standards**

- The authors declare that they have no conflict of interest.
- This article does not contain any studies with human participants or animals performed by any of the authors.
- The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.
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